

The Inadequacy of Uncertainty Estimation in Residual Stress Measurements

And some ideas on what to do about it

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Ignorance is not probabilistic.

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So we generally end up with a lower
bound estimate of uncertainty

Not conservative

Outline

- **Motivation**
- **Conventional uncertainty estimation**
- **Two examples of *demonstrably* underestimated uncertainties, with improvements proposed**
 - Incremental slitting: improving the *analytical* estimation of uncertainty
 - Neutron diffraction: improving uncertainty estimation using additional *data*
- **Thoughts**

Motivation

- **In the context of structural integrity, life prediction, and structural health monitoring, for example, ...**
- **Uncertainties *on the important quantities* ...**
 - Lifetime, crack growth rate, stress corrosion cracking rate,

Are vital for protecting human life and assets while minimizing cost/weight/inspections, etc.
- **For the purposes of this talk, we assume that uncertainties on residual stress measurements and/or predictions are a necessary part of that**

Standard uncertainty

- **The overwhelming majority of uncertainty estimates come from the standard error propagation equation**

Let $f(x,y)$ be a function of two variables, and assume that the uncertainties on x and y are known and “small”. Then:

$$\sigma_f^2 = \left(\frac{df}{dx}\right)^2 \sigma_x^2 + \left(\frac{df}{dy}\right)^2 \sigma_y^2 + 2 \left(\frac{df}{dx}\right) \left(\frac{df}{dy}\right) \rho \sigma_x \sigma_y$$

(Note that I have included the cross-terms, which cannot always be ignored)

- **Where we propagate the uncertainty in the main measured quantity (e.g., strain, diffraction peak location, ...) and usually nothing else**

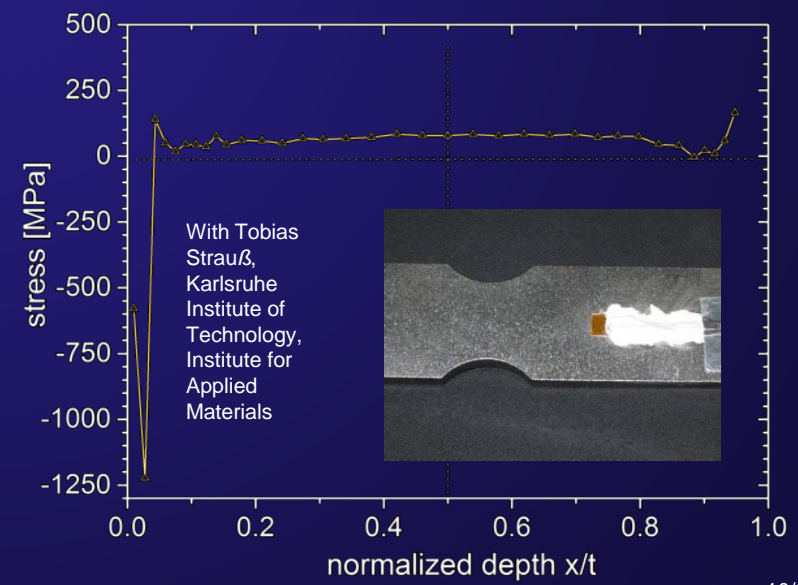
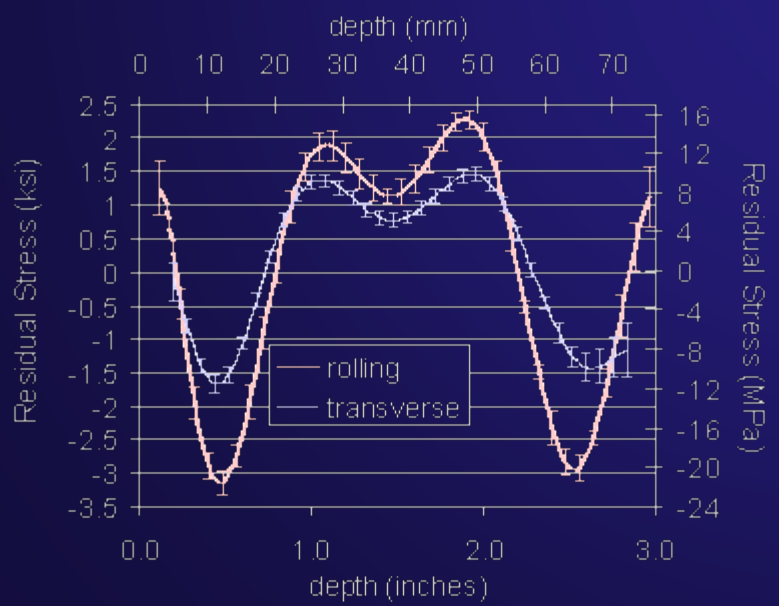
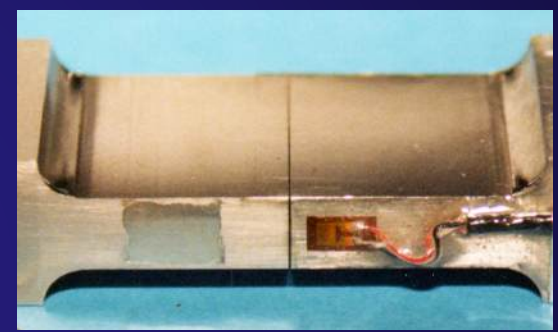
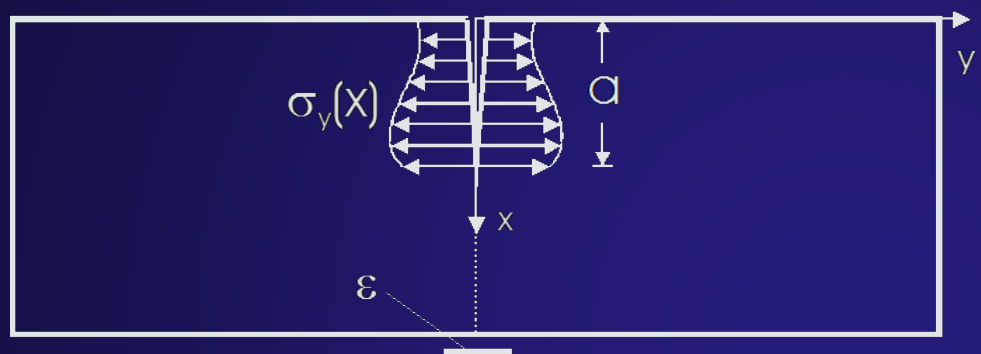
This approach is often inadequate for two reasons:

1. We do not propagate all of the uncertainties
2. This approach is inadequate in itself

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The slitting method is a powerful tool for measuring a depth profile of residual stresses



Uncertainty propagation through least squares fit inverse

$$\sigma_y(x_i) = \sigma_i = \sum_{j=1}^n A_j P_j(x_i) = [P]\{A\}$$

$$\{A\} = \left[\left([C]^T [C] \right)^{-1} [C]^T \right] \{\varepsilon\} = [B]\{\varepsilon\}$$

$$s_i^2 = u_{A_1}^2 \left(\frac{\partial \sigma_i}{\partial A_1} \right)^2 + u_{A_2}^2 \left(\frac{\partial \sigma_i}{\partial A_2} \right)^2 + \dots + 2u_{A_1 A_2}^2 \left(\frac{\partial \sigma_i}{\partial A_1} \right) \left(\frac{\partial \sigma_i}{\partial A_2} \right) + \dots$$

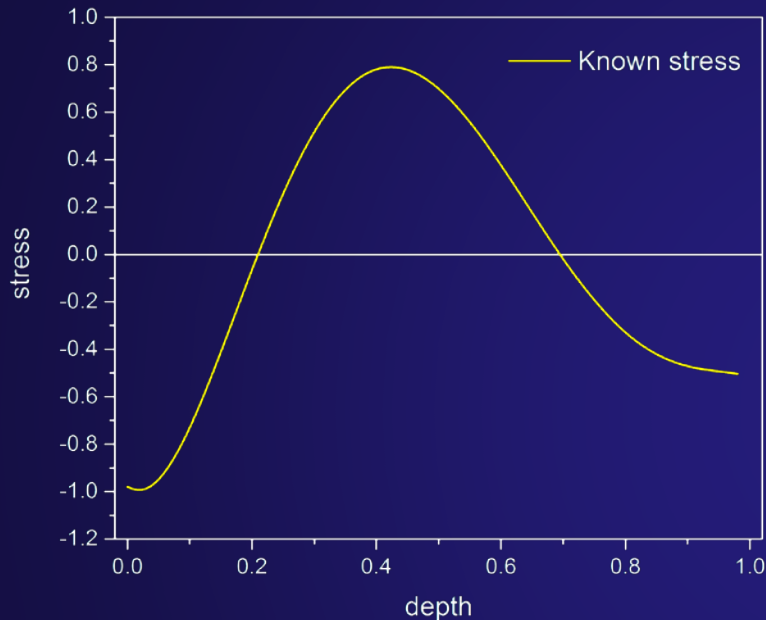
$$\frac{\partial \sigma_i}{\partial A_j} = P_j(x_i) \quad \{s_i^2\} = \text{diag}([P][V][P]^T)$$

$$V_{kl} = u_{A_k A_l}^2 = \sum_{i=1}^m \left[u_{\varepsilon, i}^2 \frac{\partial A_k}{\partial \varepsilon_i} \frac{\partial A_l}{\partial \varepsilon_i} \right] \quad \frac{\partial A_k}{\partial \varepsilon_i} = B_{ki} \quad [V] = [B][\text{DIAG}\{u_{\varepsilon}^2\}][B]^T$$

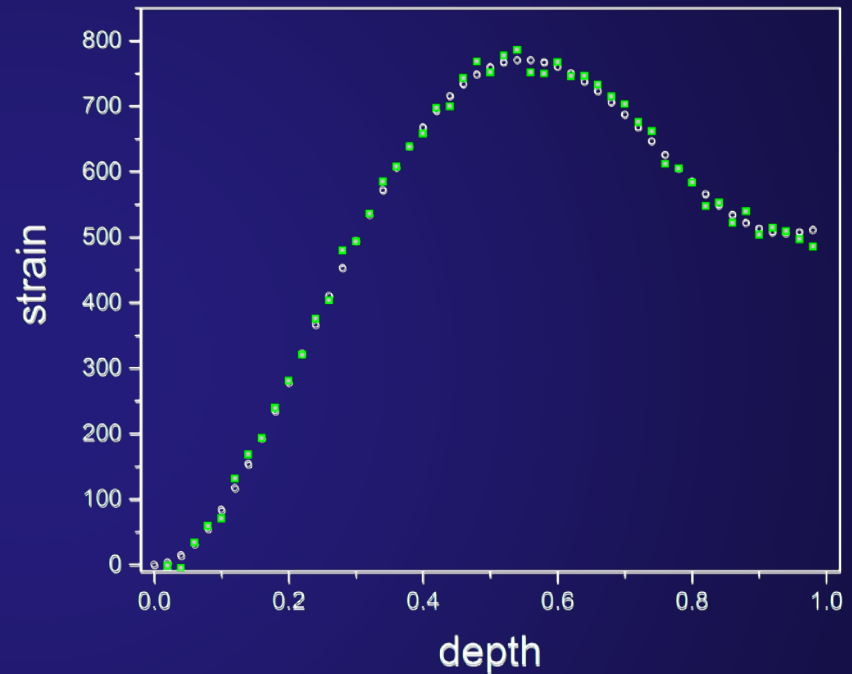
$$\{s_i^2\} = \text{diag} \left([P] \left[\left([C]^T [C] \right)^{-1} [C]^T \right] [\text{DIAG}\{u_{\varepsilon}^2\}] \left[\left([C]^T [C] \right)^{-1} [C]^T \right] [P]^T \right)$$

Let's test it analytically

- Pick a test stress profile

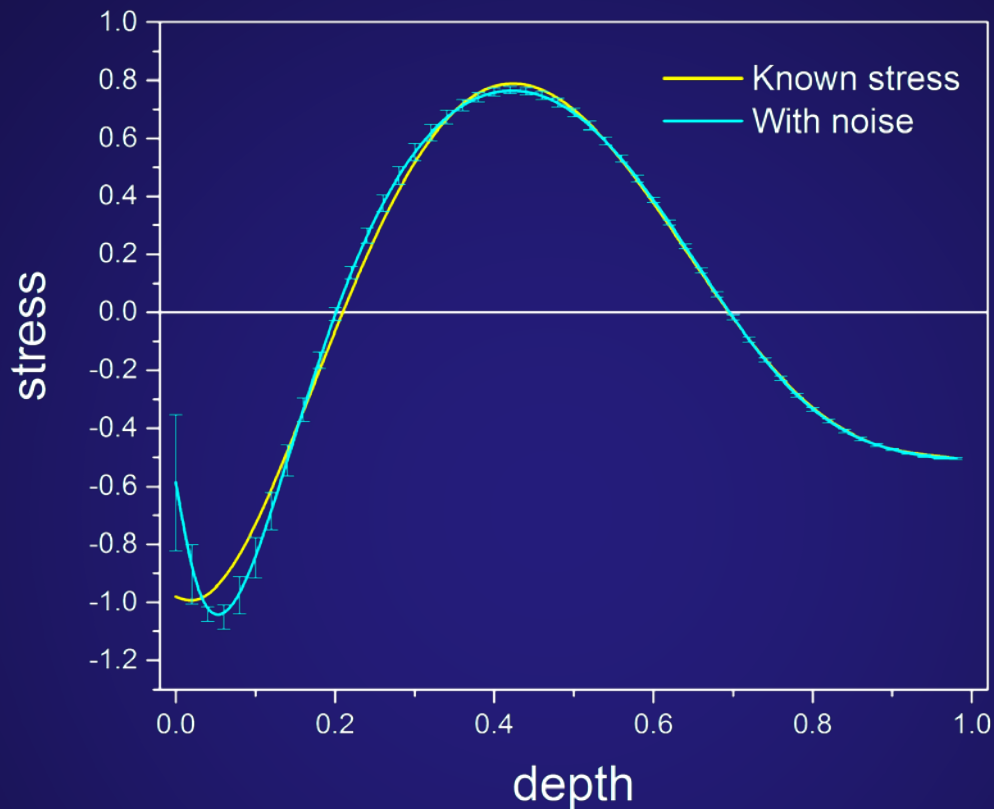


- Use FEM to generate strain "data"



- Add some Gaussian random noise to the data
- Calculate stress and estimate errors

Uncertainty analysis seems to work well



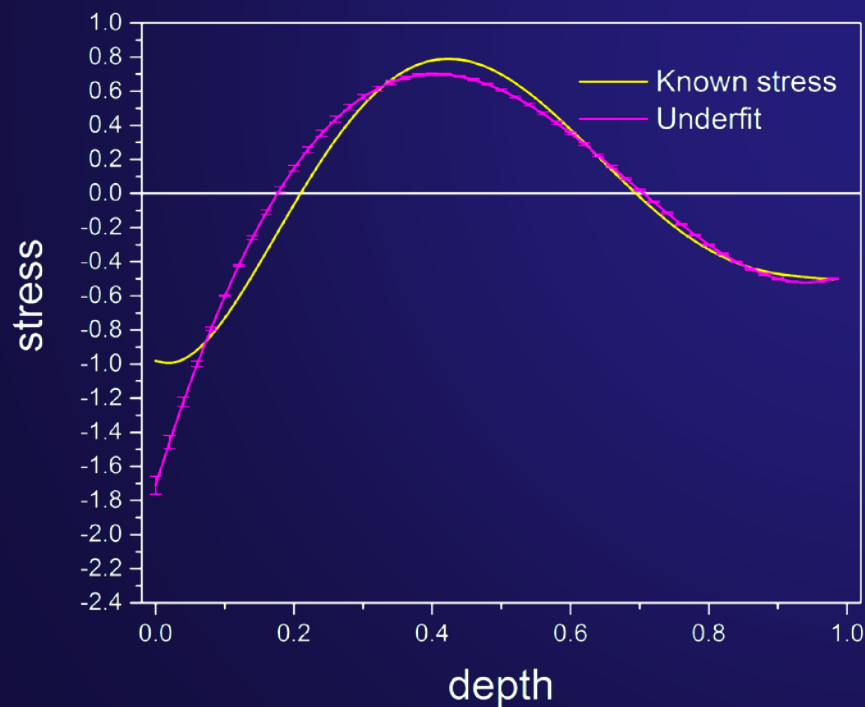
- **These are one standard deviation error bars (for the whole talk)**
 - So they should only encompass about 68% of the distribution

The only way to test a hypothesis is to look for all the information that disagrees with it

Sir Karl R. Popper
Austrian-British philosopher of science
Proponent of falsificationism

More general case?

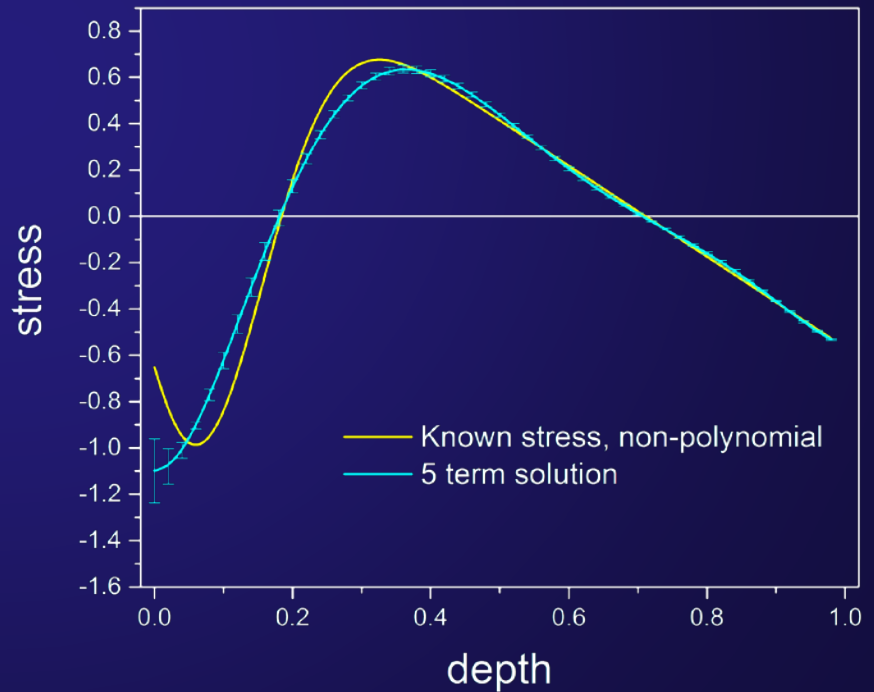
- The test case was a 4th order polynomial
- What if I solve the inverse problem with only 3rd order?
 - After all, you do not know what the “right” order is



- Or with a profile that is not polynomial at all

$$\sigma(x) = 2.28735 \left(0.609825 - 0.857365x - e^{\left(\frac{x-0.05}{0.15}\right)^2} \right)$$

- **Uncertainty is grossly underestimated**



What to do?

- We usually estimate uncertainty based on uncertainty in the measured quantity:

$$\partial \varepsilon_i$$

- But really our choice of the “model” to represent the stress profile is equally uncertain

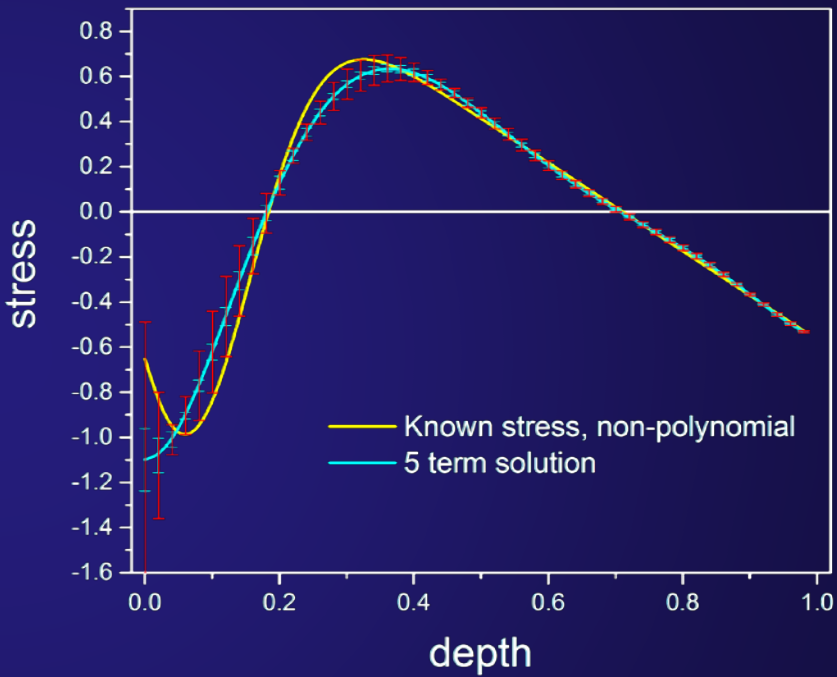
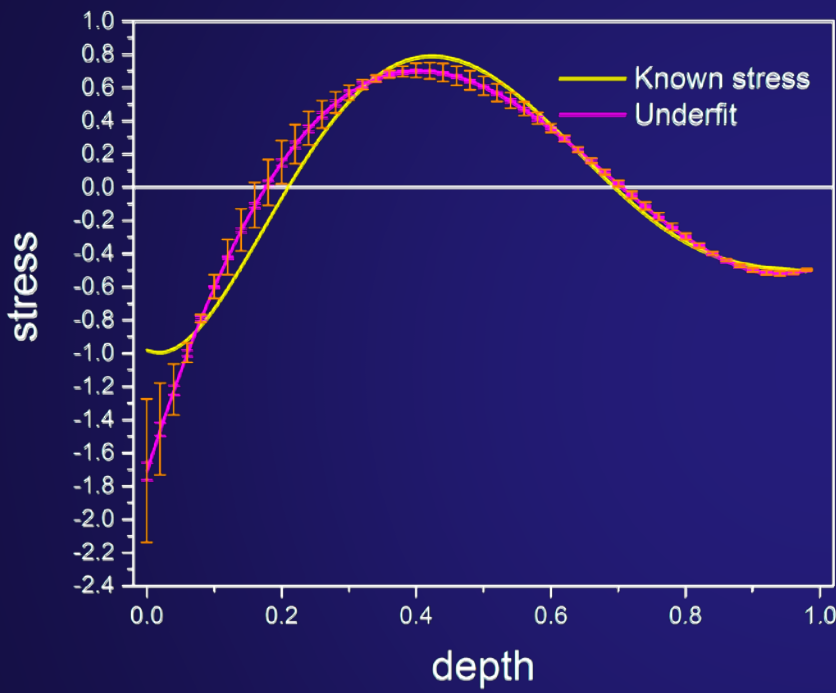
$$\sigma_y(x_i) = \sigma_i = \sum_{j=1}^n A_j P_j(x_i) = [P]\{A\}$$

- So we devised a simple model uncertainty based on the uncertainty in n

$$\partial n$$

- Just by looking at neighboring fit orders

A big improvement



Prime, M. B., and Hill, M. R., 2006, "Uncertainty, Model Error, and Order Selection for Series-Expanded, Residual-Stress Inverse Solutions," *Journal of Engineering Materials and Technology*, **128**(2), pp. 175-185.

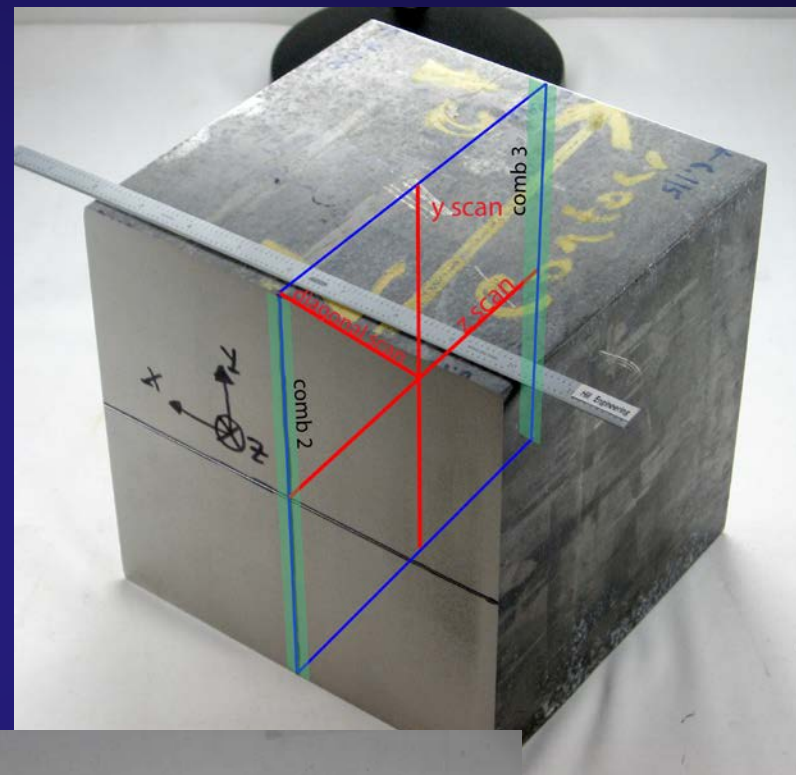
- **Looking at the easy part of uncertainty, like the strain errors, is not good enough**
- **Often the bigger error is *not* the measurement but is the *model* we use to describe our physical system**
 - Model error
- **With some effort, we can find ways to improve the uncertainty estimate for processed data**
- **Least squares fits are a great way to use more data to get a better answer**
 - But can give very low uncertainty estimates using simple propagation
 - Because errors often do not fit the model

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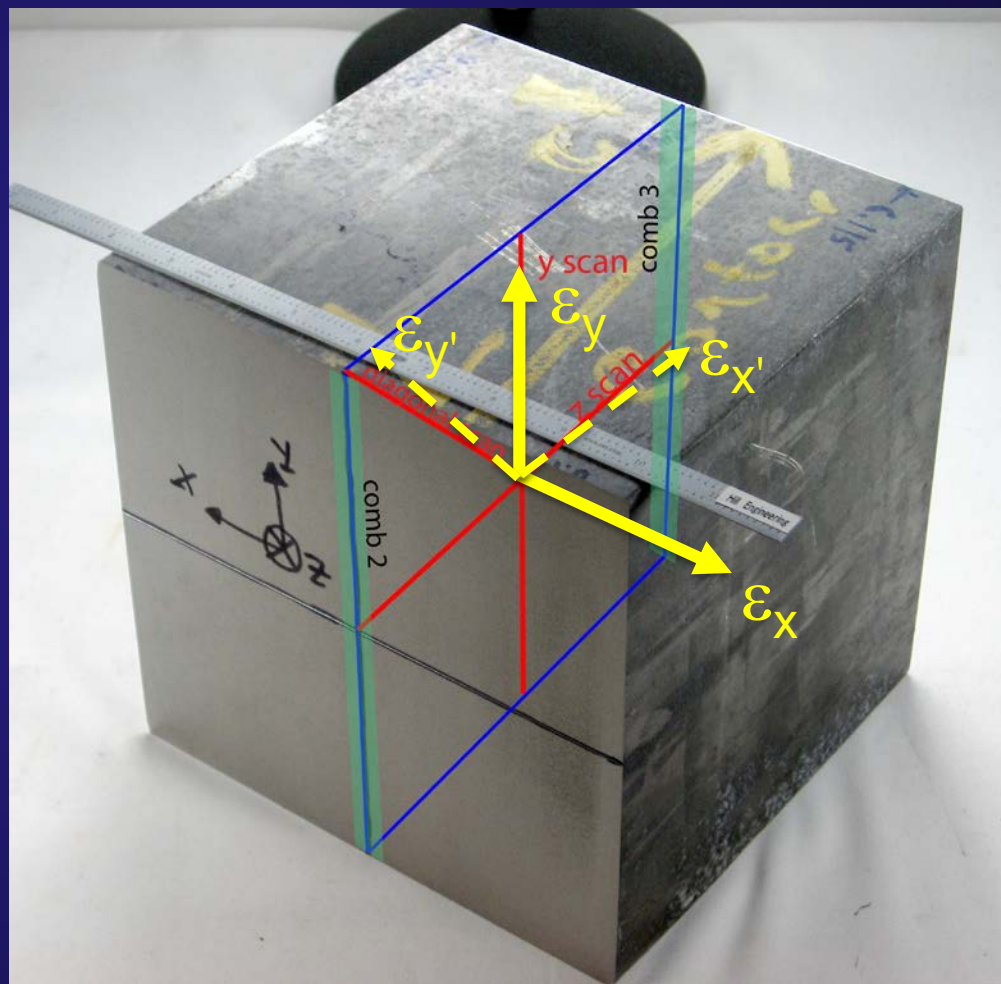
State-of-the-art neutron diffraction stress mapping on large forging

- **7050 Aluminum forging**
 - NOT stress relieved
 - $\approx 200 \text{ mm} \times 200 \text{ mm} \times 200 \text{ mm}$ section
- **Time-of-flight diffraction at SMARTS at LANL**
 - Rietveld refinement to get strains
- **Low penetration on this thick part**
 - So used 3 scan lines to get a reasonable map over cross-section
 - Big sampling volume
 - 5 x 5 mm slits
 - 4 mm collimators
 - Took ~ 120 hours
- **Used combs to get stress-free reference (d_0)**



Additional neutron orientation to get ϵ_{xy}, τ_{xy}

- As is standard, used two orientations to get 3 ϵ 's and therefore σ in x - y - z directions
- We were also interested in x - y shear stresses
 - So added an orientation at 45° in x - y plane

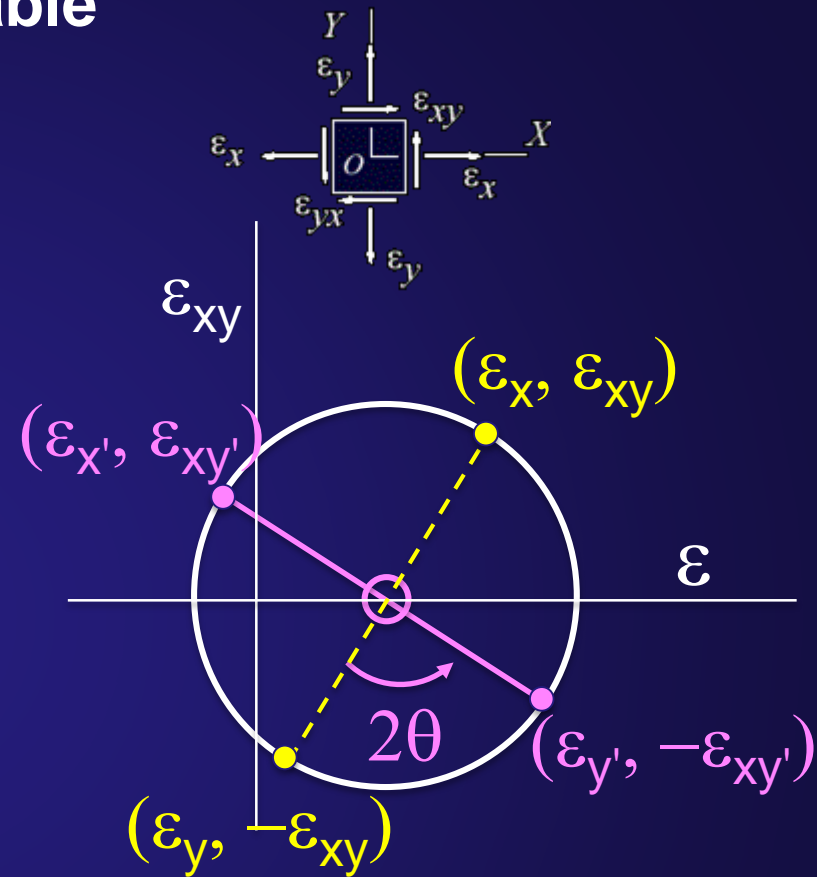


Redundant data gives an inviolable check on correctness of results

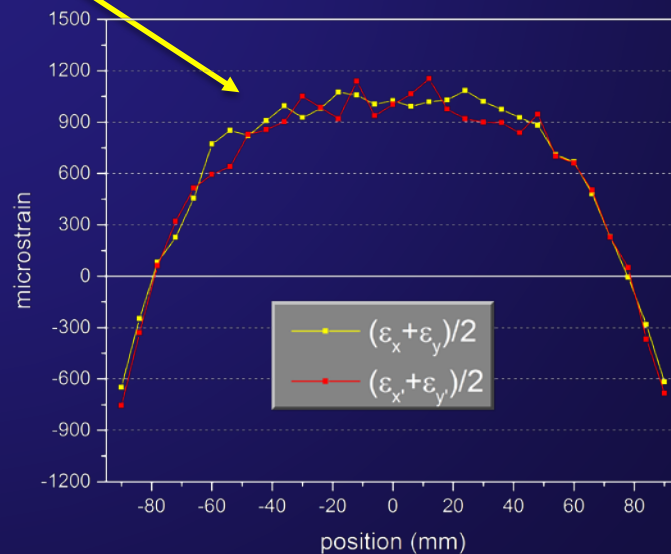
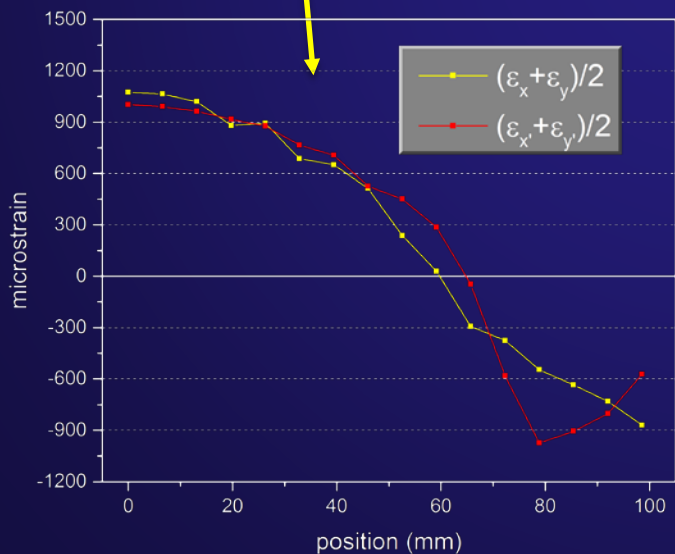
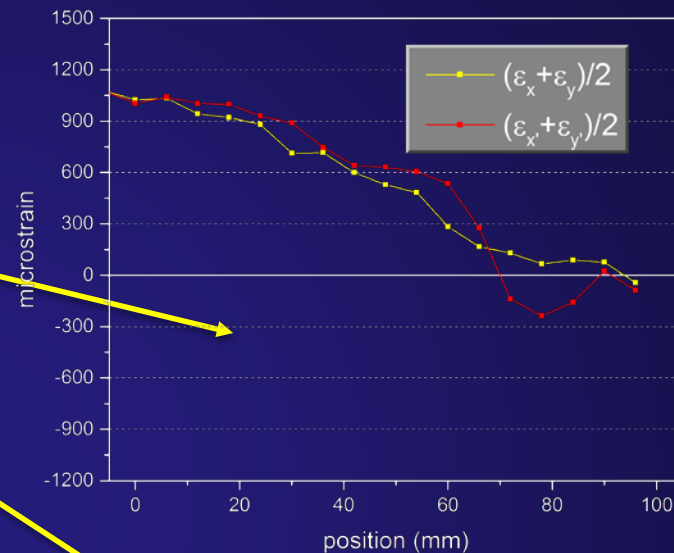
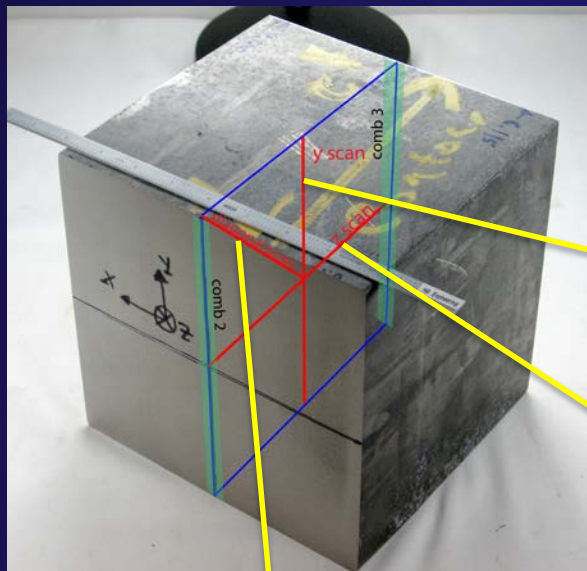
- We have redundant information
 - It only takes three in-plane strains to determine the whole in-plane strain state
 - We have 4
- Mohr's circle is a convenient graphic construct of in-plane strains
- Can be used to rotate strain state
- Gives an easy consistency check:
 - The center of the circle is always the same

$$\frac{\epsilon_x + \epsilon_y}{2} = \frac{\epsilon_{x'} + \epsilon_{y'}}{2}$$

- (rotational invariant)



How good should this agreement be?



Standard Neutron Uncertainty Calculation uses Uncertainty in Peak Fit

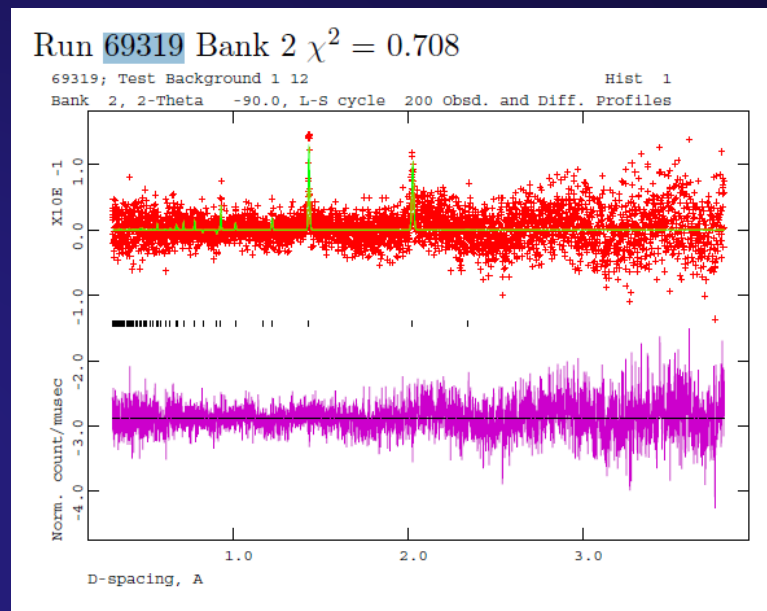
- Rietveld refinement fits diffraction peak pattern to fcc crystal structure of aluminum to give lattice parameter and uncertainty
 - $a \pm \delta a$
- Which we can propagate through all equations

$$\varepsilon = \frac{a - a_0}{a_0}$$

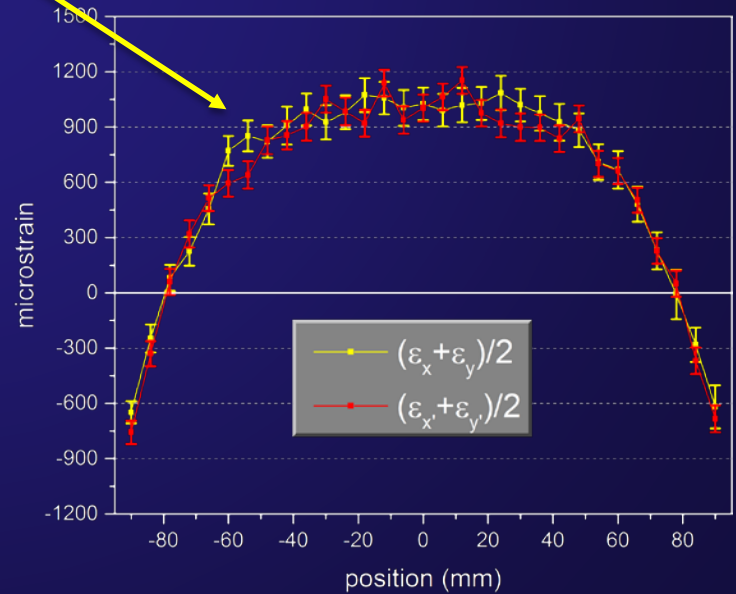
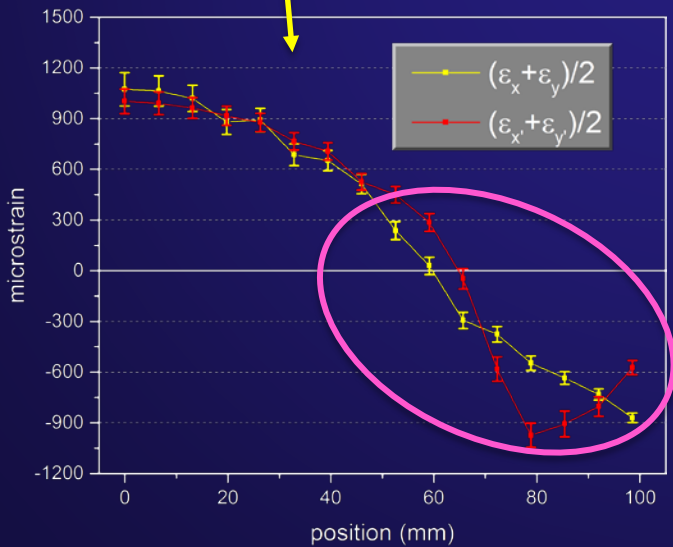
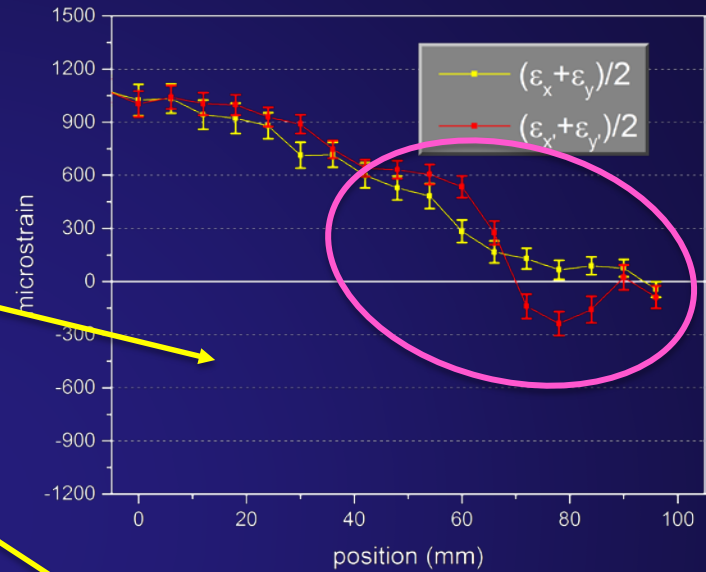
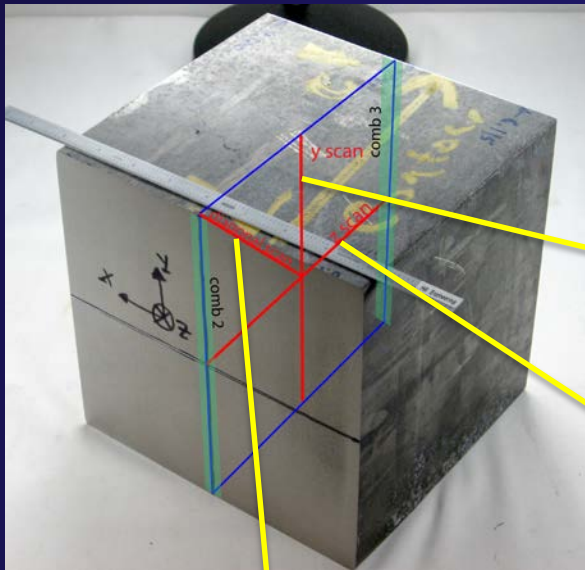
- ε uncertainty on a AND a_0

$$\sigma_i = \frac{E(1 - \nu)}{(1 + \nu)(1 - 2\nu)} \left[\varepsilon_i + \frac{\nu}{1 + \nu} (\varepsilon_j + \varepsilon_k) \right]$$

- To get $\sigma \pm \delta \sigma$
- *** I added extra uncertainty to a_0 because of uncertainty in spatial variation (which was measured)



In some regions, uncertainties are underestimated, almost by definition



Can we independently check the accuracy of the neutron results?

- The neutron measurements were motivated as a independent validation of fracture surface contour measurement
 - Spoke on this in Summit 2013
- But maybe we can learn something about the neutron accuracy with the comparison
- Contour/fracture uncertainties calculated based on
 - Olson, M. D., DeWald, A. T., Prime, M. B., and Hill, M. R., 2015, "Estimation of Uncertainty for Contour Method Residual Stress Measurements," *Experimental Mechanics*, **55**(3), pp. 577-585.

Engineering Fracture Mechanics 116 (2014) 158–171

Contents lists available at ScienceDirect

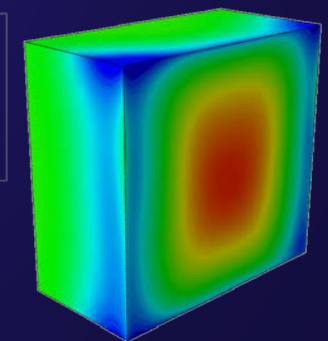
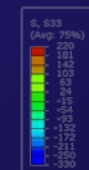
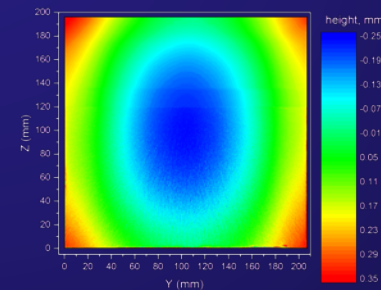
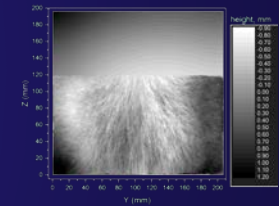
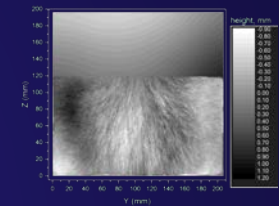
Engineering Fracture Mechanics

journal homepage: www.elsevier.com/locate/engfracmech

Forensic determination of residual stresses and K_I from fracture surface mismatch

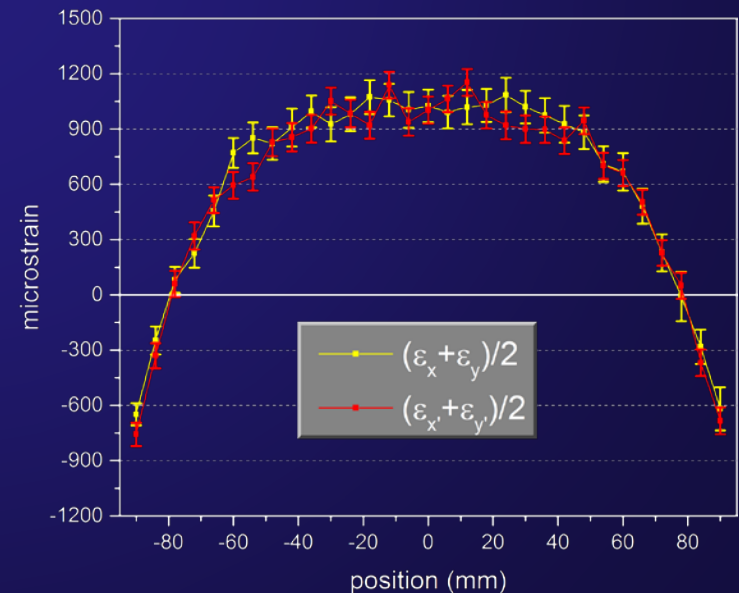
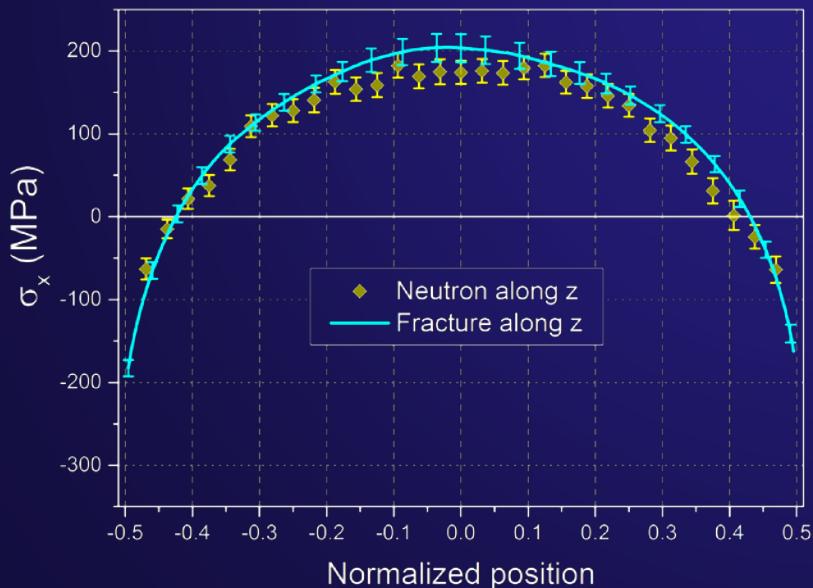
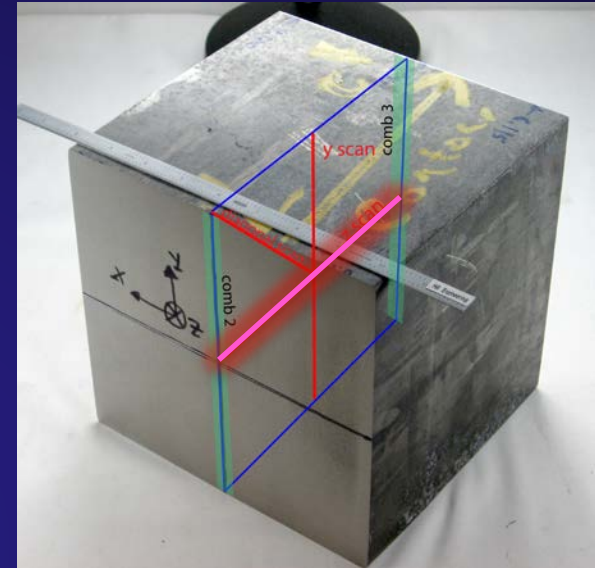
Michael B. Prime^{a,*}, Adrian T. DeWald^b, Michael R. Hill^c, Bjørn Clausen^a, Minh Tran^c

^aLos Alamos National Laboratory, Los Alamos, NM 87545, United States
^bHill Engineering, LLC, Rancho Cordova, CA 95670, United States
^cMechanical and Aerospace Engineering Department, University of California, Davis, CA 95616, United States



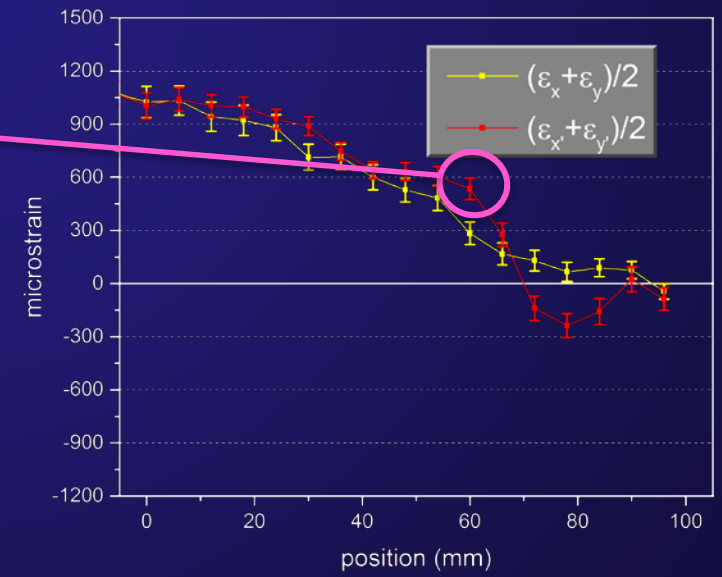
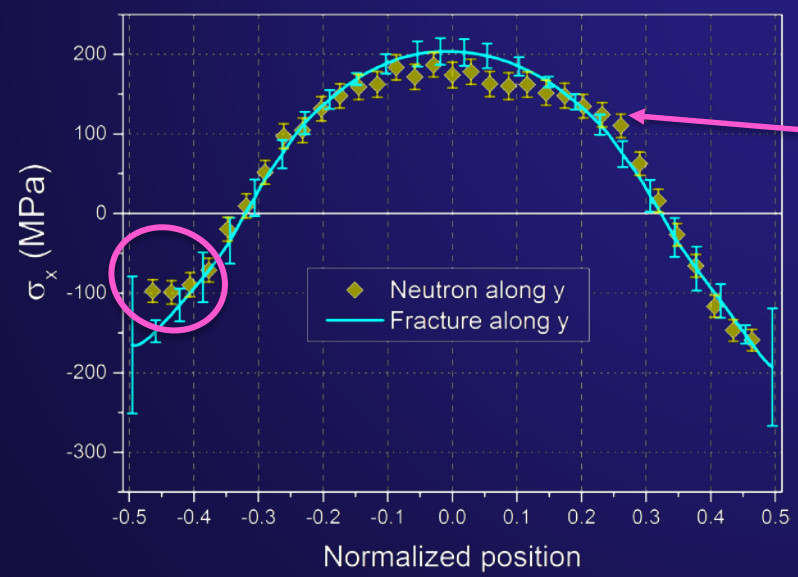
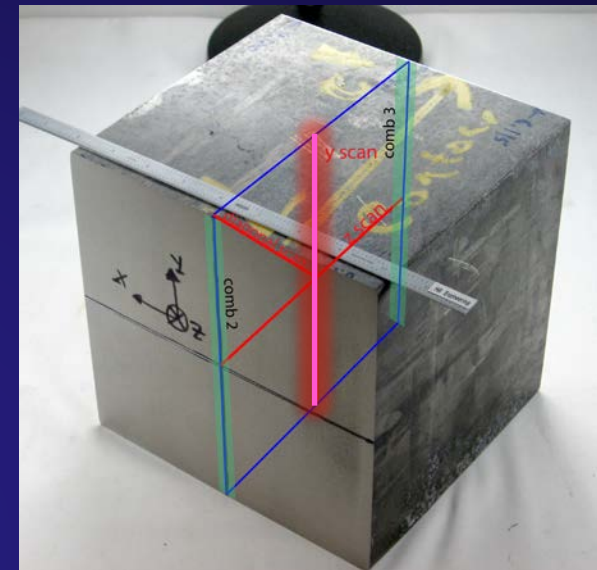
Z-scan neutron uncertainties look OK

- Neutron and fracture-surface-contour results agree within uncertainty
- And this is scan where strain consistency check also passed within uncertainty
- Interestingly, region near $z=0$ where ε 's barely passed had biggest disagreement
 - Could be a_0 bias error
 - Could probably use a bigger uncertainty



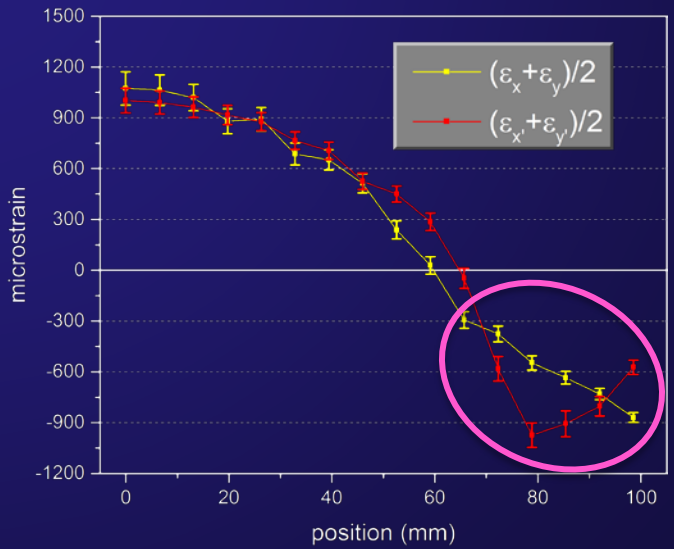
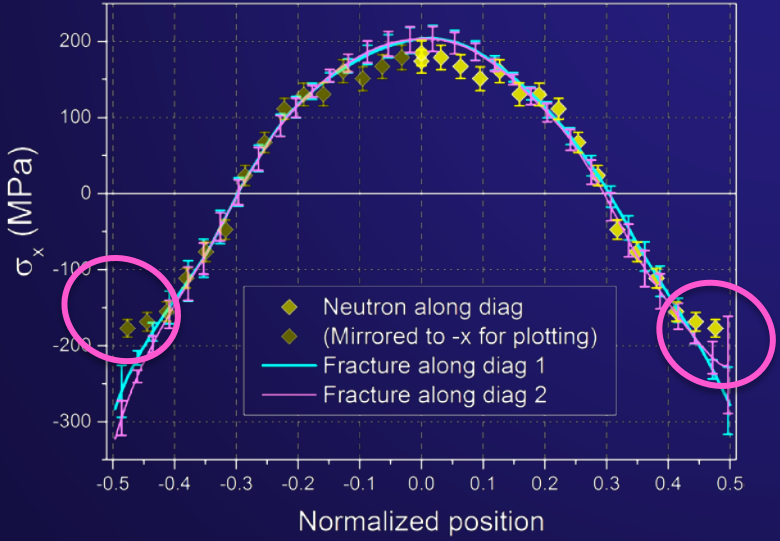
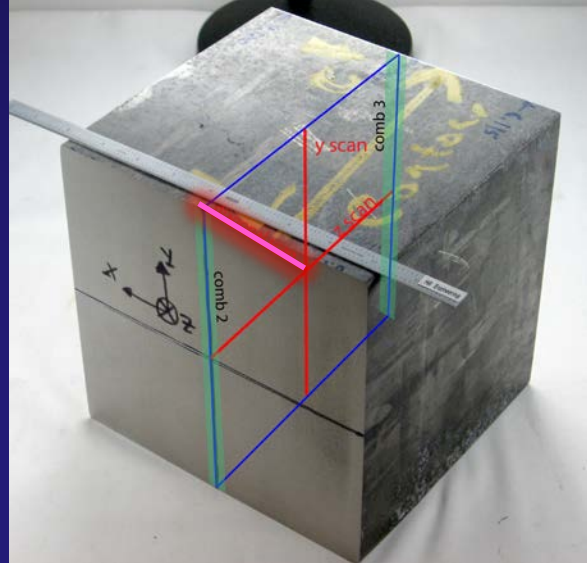
Y-scan neutron uncertainties underestimated in places

- **Uncertainties underestimated sometimes**
 - Correlates well with strain checks inconsistency
 - Even if some places with consistency have good agreement
- **Note; if I had not added additional uncertainty to a_0 , neutron error bars would be even smaller**



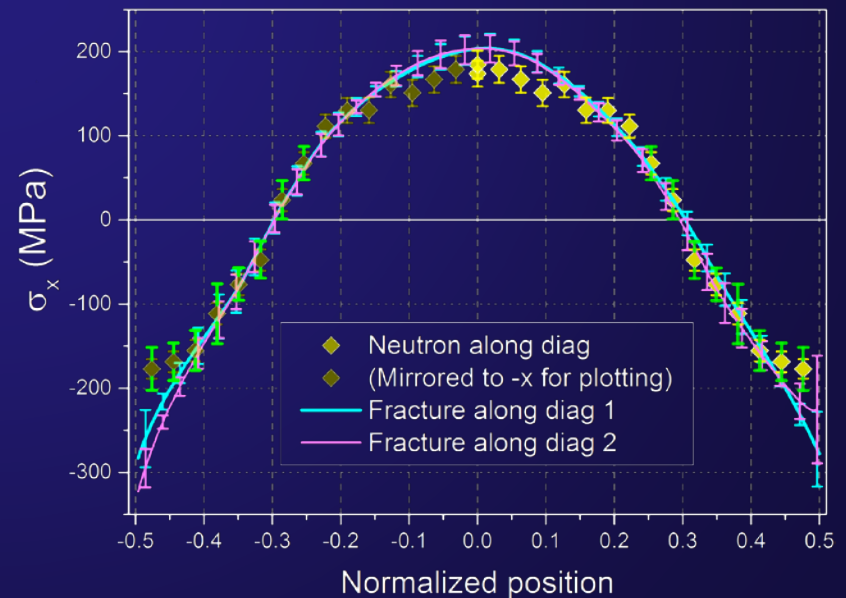
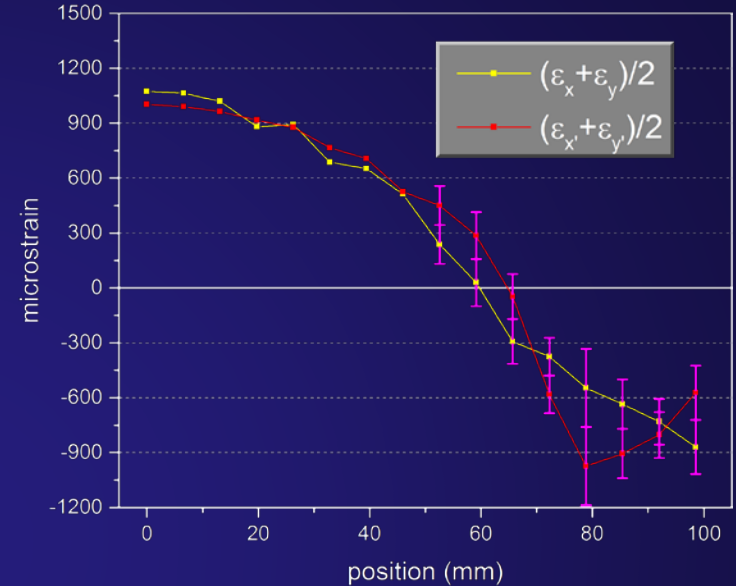
Diagonal scan neutron uncertainties

- More correlation between strain check inconsistency and disagreement between methods



One simple improvement

- **Set strain uncertainty to the *larger* of**
 - Conventionally propagated uncertainty
 - $\frac{1}{2}$ the difference in the consistency check
- **Gives us a much better uncertainty estimate for this test**
 - based on comparison to fracture surface results



Is this a practical approach?

Can we use this redundant data idea generally with neutron diffraction?

- **Requires at least one extra orientation in order to get a redundant strain**
 - Would be a 50% increase compared to usual two orientations
 - Except that you could probably get away with not doing every measurement point

- **Redundant orientations are rare, and not used this way**
 - A least squares fit is used to get a more accurate strain state - good
 - With a lower uncertainty based on the least squares fit
 - Bad if the uncertainty is less than the consistency discrepancy

Conclusions

- **Standard uncertainty propagation underestimates uncertainty more often than not**
- **Measurement providers can do several things to improve uncertainty estimates**
 - Data driven
 - Take redundant data in order to check and if necessary increase uncertainties
 - Repeat measurements to establish repeatability-based uncertainty
 - Multiple method comparisons
 - Repeat measurements with changes
 - Contour cut in other direction
 - Different diffraction peak
 - Analysis
 - Include more uncertainty sources in error propagation
 - Include alternate uncertainty estimates
- **Users can also contribute**
 - Insist on documented uncertainty estimate
 - But you have to pay for it
 - Support repeats and other studies to better establish uncertainty